# Structural, Elastic and Electronic Properties of $\gamma''$ Phase Precipitate in Mg-Gd-Zn Alloy

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**Summary:** The  $\gamma''$  phase (Mg<sub>4</sub>GdZn) precipitate in Mg-Gd-Zn alloy was calculated via first-principle density functional theory within the generalized gradient approximation. Through structure optimization of full relaxation, the lattice parameters were theoretically obtained, and the calculated Mg<sub>4</sub>GdZn is the most energetically stable in view of the formation energy. Independent elastic constants were also calculated, illustrating the calculated Mg<sub>4</sub>GdZn is mechanically stable. The shear modulus, polycrystalline bulk modulus, Poisson ratio, and Young's modulus of Mg<sub>4</sub>GdZn were calculated via the Voigt-Reuss-Hill approximation. Elastic anisotropy and ductility were analyzed in details. Seen from their charge density distribution and electronic density of states, both metallic bond and covalent bond were found in Mg<sub>4</sub>GdZn.

Keywords: First-principles calculations; Elastic properties; Elastic anisotropy; Electronic structure;  $\gamma$ " phase; Mg<sub>4</sub>GdZn.

#### Introduction

Various rare-earth-containing magnesium alloys, for example, Mg-Y-Nd, Mg-Gd-Y, and Mg-Gd-Nd, have been receiving more and more attention in recent years due to their better creep resistance and higher strength [1-9]. For the Mg-Gd-based systems,  $\beta'$  and  $\beta_1$  are the key strengthening precipitate phases, and the precipitation sequence and structure, morphology of these phases in the mentioned systems have been relatively established. For binary Mg-Gd alloy with content of Gd<1.4 at.%, it shows little age hardening response. The phenomenon is resulted from the lack of obvious volume fraction of precipitates and even the rare distribution of coarse precipitates. Fortunately, the addition of slight amount of Zn (0.5-0.7 at.%) could produce an intensive precipitation hardening response and sharply increase the alloy creep resistance [10]. Moreover, the hardness of the alloy is also greatly enhanced (~17 VHN), even when quenching. The improvement of the alloy is remarkable when the content of Zn is 0.4 at.%. A recent study has demonstrated that the enhancement of age hardening response results from a denser distribution of  $\gamma''$  phase precipitate that is not found in binary Mg-Gd alloy.

Through the 3-dimensional atom probe and selected area electron diffraction analysis, Nie has proposed Mg<sub>4</sub>GdZn as the chemical composition of  $\gamma''$ 

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phase precipitate, and constructed a hexagonal unit cell as the concrete structure model [11]. Based on the crystal structure in  $\alpha$ -Mg, Nie has deduced an ordered hexagonal structure (space group P62m, a = 5.60 Å, c =4.44 Å) of the  $\gamma''$  phase. However, the result has not been confirmed, no matter theoretically or experimentally. Besides, as a key strengthening phase in the Mg-based alloy, the  $\gamma''$  precipitate has great significance in optimizing the micro-structure and enhancing their mechanical properties. Unfortunately, the investigation about the  $\gamma''$  precipitate is relatively rare. Therefore, further theoretical and experimental studies are imperative.

In this paper, theoretical calculations based on first-principle within the generalized gradient approximation (GGA) were performed to study the elastic property and electronic structure of the  $\gamma''$  phase (Mg<sub>4</sub>GdZn) in Mg-Gd-Zn system. The results were analyzed and compared to the experimental data reported in literatures, which can provide references for the rational design and optimization of Mo-based alloys.

# Experimental

Calculations were completed through the Vienna Ab Simulation Package [12]. The Perdew-Wang (PW91) version of the GGA [13] and the projector augmented wave method [14] were adopted. The cutoff

energy for the plane wave basis set was 360 eV and Gamma centered Monkhors-Pack grids with  $12 \times 12 \times 15$  for the BZ integration were adopted [15].

Elastic constants were obtained through the calculation of the total energy as a function of proper lattice deformation, and internal energy  $E(V, \varepsilon)$  for the slightly deformed crystal is calculated by Equation (1) [16].

$$E(V, [\varepsilon_{mn}]) = E(V_0, 0) + \frac{V_0}{2} \sum_{i,j=1}^{6} c_{ij} \varepsilon_i \varepsilon_j \qquad (1)$$

where  $E(V_0, 0)$  is the total energy in equilibrium, and  $\varepsilon_i$  and  $\varepsilon_i$  are strains with Voigt's notation.

The five independence elastic constants were calculated through fitting the energy-strain profiles with quadratic polynomial which can be found in details in Ref. [17-19].

#### **Results and Discussion**

#### Crystal structure and stability

Mg<sub>4</sub>GdZn shows a hexagonal structure with a P62m space group. Based on the structure model proposed by Nie [11], we performed the structure optimization through the relaxation of internal atom positions and unit cell shape. The equilibrium lattice parameters of Mg<sub>4</sub>GdZn are a=b=5.646 Å, c=4.783 Å. In comparison with the experimental value (a=b=5.60 Å, c=4.44 Å, see Ref. [11]), the present theoretical lattice parameters a and b are in accordance with the expected value from the structure model, while c is larger evidently. The reason lies in the different atom radii of Mg (1.60 Å) and Gd (1.88 Å). Hence, the lattice parameters of the alloys will change due to the addition of Gd. The obtained results here will shed a light on the further theoretical and experimental investigation of the alloy. In addition, a series of total energies per unit cell were also obtained and fitted by the Birch-Murnaghan equation of state (EOS) [19]. The volume  $V_0$  and bulk modulus  $B_0$  are 138.6 Å<sup>3</sup> and 42.54 GPa, respectively.

The formation energy was further calculated by Equation (2) in order to investigate the structure stability of the  $Mg_4GdZn$ . The obtained formation energy for

 $Mg_4GdZn$  is -0.084 eV/atom, and the negative formation energy proves the formation stability of  $Mg_4GdZn$ .

$$\Delta H = \frac{E_{tot} - N_A E_{solid}^A - N_B E_{solid}^B - N_C E_{solid}^C}{N_A + N_B + N_C}$$
(2)

#### Elastic properties

Table-1 showed the calculated elastic constants which can provide useful information of bonds in the material and are closely related to the mechanical properties. In Mg4GdZn, the elastic constant  $C_{11}$  is less than  $C_{33}$ . On one hand, it illustrates the weaker bond strength along directions [1010] and [0110] than that along [0001]. On the other hand,  $C_{11}+C_{12}>C_{33}$ implies the higher elastic modulus in (0001) plane than along c-axis [20]. Besides,  $C_{44}$  is higher than  $C_{66}$ , indicating that the easier shear of [1010] (0110) than that of [1010] (0001). The mechanical stability criteria of hexagonal lattice are  $C_{11}$ ,  $C_{11}$ - $C_{12}$ ,  $C_{44}$  and  $(C_{11}+C_{12})C_{33}-2C_{13}^2$  must be positive [21]. The calculated elastic constants of Mg4GdZn obeyed are in line with the criteria, illustrating the mechanical stability of Mg<sub>4</sub>GdZn.

The polycrystalline elastic modulus was also determined [22]. For the hexagonal cell, the Voigt limits of  $G(G_V)$  and  $B(B_V)$  are shown in Equations (3-4).

$$G_{V} = \frac{1}{30} \left( 7C_{11} - 5C_{12} + 12C_{44} + 2C_{33} - 4C_{13} \right)$$
(3)

$$B_V = \frac{2}{9} \left( C_{11} + C_{12} + C_{33} / 2 + 2C_{13} \right) \tag{4}$$

And the Reuss bounds ( $G_R$  and  $B_R$ ) are shown in Equations (5-6).

$$G_{R} = \frac{5}{2} \left\{ \frac{\left[ (C_{11} + C_{12})C_{33} - 2C_{13}^{2} \right]C_{44}C_{66}}{3B_{V}C_{44}C_{66} + \left[ (C_{11} + C_{12})C_{33} - 2C_{13}^{2} \right](C_{44} + C_{66})} \right\}$$
(5)  
$$B_{R} = \frac{(C_{11} + C_{12})C_{33} - 2C_{13}^{2}}{C_{11} + C_{12} + 2C_{33} - 4C_{13}}$$
(6)

Table-1: Single crystal elastic constants  $c_{ij}$  (in GPa), elastic modulus (in GPa) and Poisson's ratio v of Mg<sub>4</sub>GdZn.

C11	$C_{12}$	C <sub>33</sub>	C <sub>13</sub>	C44	C <sub>66</sub>	$C_{11}$ - $C_{12}$	В	G	Y	v
68.86	31.77	86.28	29.93	34.06	18.55	37.09	45.07	25.22	63.76	0.26

Ultimately, the mean values of VRH are calculated by Equations (7-8).

$$B = \frac{1}{2}(B_V + B_R) \tag{7}$$

$$G = \frac{1}{2}(G_V + G_R) \tag{8}$$

where the subscripts V and R are the Voigt and Reuss bounds, respectively. Furthermore, the Young's modulus Y and Poisson's ratio v are calculated according to Equations (9-10).

$$Y = \frac{9BG}{3B+G} \tag{9}$$

$$v = \frac{3B - 2G}{2(3B + G)}$$
(10)

The calculated results were also shown in Table-1. It is noted that the obtained bulk modulus of Mg<sub>4</sub>GdZn is in accordance with that obtained by fitting to the Birch-Murnaghan EOS. Elastic moduli can determine the hardness of material. Elastic moduli include bulk modulus, shear modulus and Young's modulus [23, 24]. Fig. 1 showed the obtained shear modulus, bulk modulus and Young's modulus comparing with the corresponding experimental values in single-crystal Mg [25]. The obtained bulk modulus of Mg4GdZn is higher obviously than the experimental value of Mg, and the enhancement implies higher hardness of the material, which is in line with the reported experiment values [11]. Besides, the evident enhancements of Young's modulus and shear modulus of Mg<sub>4</sub>GdZn were also found, indicating the better mechanical property in Mg<sub>4</sub>GdZn.

Pugh proposed a general B/G criterion to predict the ductility or brittleness of material [26]. A higher B/G value is related to ductility, and the criterion distinguishing ductility and brittleness is 1.75. Actually, the obtained value of B/G for Mg4GdZn is 1.79, slightly higher than the criterion, indicating that Mg4GdZn is ductile. Meanwhile,  $C_{11}$ - $C_{12}$  is also a very significant indicator of the mechanical property [27]. The smaller of  $C_{11}$ - $C_{12}$ , the better of the plasticity. As shown in Table-1, the  $C_{11}$ - $C_{12}$  of Mg4GdZn is lower than that of Mg, implying a good plasticity. Finally, the smaller Poisson's ratio in Table-1 also demonstrated the stability of Mg<sub>4</sub>GdZn.



Fig. 1: The elastic modulus of Mg (the experimental data from Ref. [25]) and  $Mg_4GdZn$  (the calculated values in the present work).

#### Elastic anisotropy

The elastic anisotropy of materials is related to the occurrence of micro-cracks [28]. Actually elastic anisotropic behavior is found in all of the known crystals. Hence, it is necessary to quantify the elastic anisotropy of Mg<sub>4</sub>GdZn. Here, the anisotropy of Mg<sub>4</sub>GdZn was discussed based on several criteria.

For hcp system, the linear bulk moduli  $B_a$  and  $B_c$  along *a*- and *c*-axe, respectively, are defined as Equations (11-14) [29], and the value of 1 demonstrates elastic isotropy of the material. The calculated  $B_a$  and  $B_c$  in Table-2 showed that the bulk moduli of Mg<sub>4</sub>GdZn deviate from isotropy in these two directions.

$$B_a = a \frac{dp}{da} = \frac{\Lambda}{2+\beta} \tag{11}$$

$$B_c = c \frac{dp}{dc} = \frac{B_a}{\beta} \tag{12}$$

where

$$\Lambda = 2(C_{11} + C_{12}) + 4C_{13}\beta + C_{33}\beta^2$$
(13)

$$\beta = \frac{C_{11} + C_{12} - 2C_{13}}{C_{33} - C_{13}} \tag{14}$$

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Material	$A_{\{10\bar{1}0\}}$	$A_{\{01\overline{1}0\}}$	$A_{\{0001\}}$	$A_G(\%)$	$A_{\scriptscriptstyle B}(\%)$	Ba	Bc	$1/\beta$		
Mg4GdZn	1.429	1.429	1.0	3.731	0.390	122.275	169.022	1.382		
	(a)	50 -50 -25	0 25	50 ab	(b) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c					
	-0.4 50 25									
	(c) $-25$ ac plane $25$ $-25$									

Table-2: Shear anisotropic factors, linear bulk modulus Ba (in GPa) and Bc (in GPa), and the percent of anisotropy in the compression AB and shear AG (in %).

# Fig. 2: (a) Directional dependence of Young's modulus, (b) and (c) plane projections of the directional dependence of Young's modulus in Mg<sub>4</sub>GdZn (in GPa).

The elastic anisotropy in compressibility and shear could be also qualified by two dimensionless quantities  $A_B = (B_V - B_R)/(B_V + B_R)$  and  $A_G = (G_V - G_R)/(G_V + G_R)$ , respectively [30-31]. The value of 0 means elastic isotropy while 1 shows the largest possible anisotropy. The calculated  $A_B$  and  $A_G$ are 0.39% and 3.73%, respectively, indicating a small anisotropy in Mg<sub>4</sub>GdZn.

To further describe the elastic anisotropy of Mg<sub>4</sub>GdZn, it is necessary to study the in-plane anisotropy. For hexagonal symmetry cell, the in-plane anisotropy of *a*-*b* doesn't exist while that of *a*-*c* exists [32]. Besides, the directional dependence of Young's modulus 1/Y, which is defined as Equation (15) [21], can also describe the in-plane elastic anisotropy.

$$\frac{1}{Y} = (1 - l_3^2)^2 s_{11} + l_3^4 s_{33} + l_3^2 (1 - l_3^2) (2s_{13} + s_{44})$$
(15)

The 1/Y was calculated and shown in Fig. 2. For an isotropic system, 1/Y is spherical shape. However, the nonspherical nature of 1/Y of Mg<sub>4</sub>GdZn in Fig. 2 clearly showed the anisotropy in the *ac* plane.

#### Electronic structures

In this paper, the electronic structure was also obtained to provide a better understanding of the bonding characteristic of Mg4GdZn, and to further interpret the mechanism of elastic property and structure stability of the Mg4GdZn. The DOS of Mg4GdZn was presented in Fig. 3, consisting of the DOS of Mg, Gd and Zn. Seen from the partial and total DOS shown in Fig. 3, Mg4GdZn exhibits metallic behavior. The total DOS near the Fermi level is mainly the Mg-p, Gd-d and Zn-p states, while the Gd-p and Gd-s states are weak. Near the Fermi level, a strong hybridization of Mg-p states with Zn-p, Gd-d states is found. In addition, a quasigap near the Fermi level is also found, indicating the formation of the directional covalent bond [33]. The covalent bond can raise the material strength compared to the metallic bond. Hence, the quasigap near the Fermi level indicates a pronounced stability in the alloy.



Fig. 3: The total and partial density of states of Mg<sub>4</sub>GdZn in which the Fermi level is set at zero energy and marked by the vertical dot line.

The charge density distribution of Mg<sub>4</sub>GdZn in the plane (1121) was presented in Fig. 4. The contour lines were plotted from 0.02 to 0.22 eV/Å<sup>3</sup>. The high charge accumulation between Zn and Gd atoms, together with the aspherical shape indicated directional covalent bond between the atoms. Different from the Zn-Gd bond, no overlaps of electron distribution around Mg atoms are found. Hence, the electron distribution near Mg atoms is almost metal-like bond, which is in line with the DOS analysis.



Fig. 4: The charge density distribution map on (1121) plane for  $Mg_4GdZn$  in which the contour lines are plotted from 0.02 to 0.22  $e/Å^3$  with 0.01  $e/Å^3$  intervals.

# Conclusion

In this paper, the structural, mechanical and electronic properties of Mg<sub>4</sub>GdZn in Mg-Gd-Zn alloy were studied through DFT within the GGA. The lattice parameters of Mg<sub>4</sub>GdZn were calculated theoretically, and the formation enthalpy indicates that Mg<sub>4</sub>GdZn is energetically stable. The calculated five independent elastic constants proved that Mg<sub>4</sub>GdZn is mechanically stable. The elastic anisotropy and the electronic properties were discussed in details. These results can provide references for the rational design and optimization of Mo-based alloys.

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